



Slurry Suspension

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What We Know about Mechanical Agitation

- **Thoroughly studied for 40 years**
- **Characteristics**
 - **off-bottom suspension**
 - **on-bottom motion**
 - **uniform suspension**
 - **cloud height**
- **Visual observation**
- **Reliable means of measurement**



What We Don't Know about Pulse Jet Mixers

- We don't know how a pulse will effect solids suspension**
- Pulsed operation will not be better than continuous agitation**
- We need to know about the effects of geometry on solids suspension**
- We need to know how to scale-up**



Everything We Know about Solids Suspension is Scale-up

- **All of solids suspension is empirical**
- **Observation of suspension characteristics**
- **Testing in different scales**
- **Scale-up of small-scale tests**

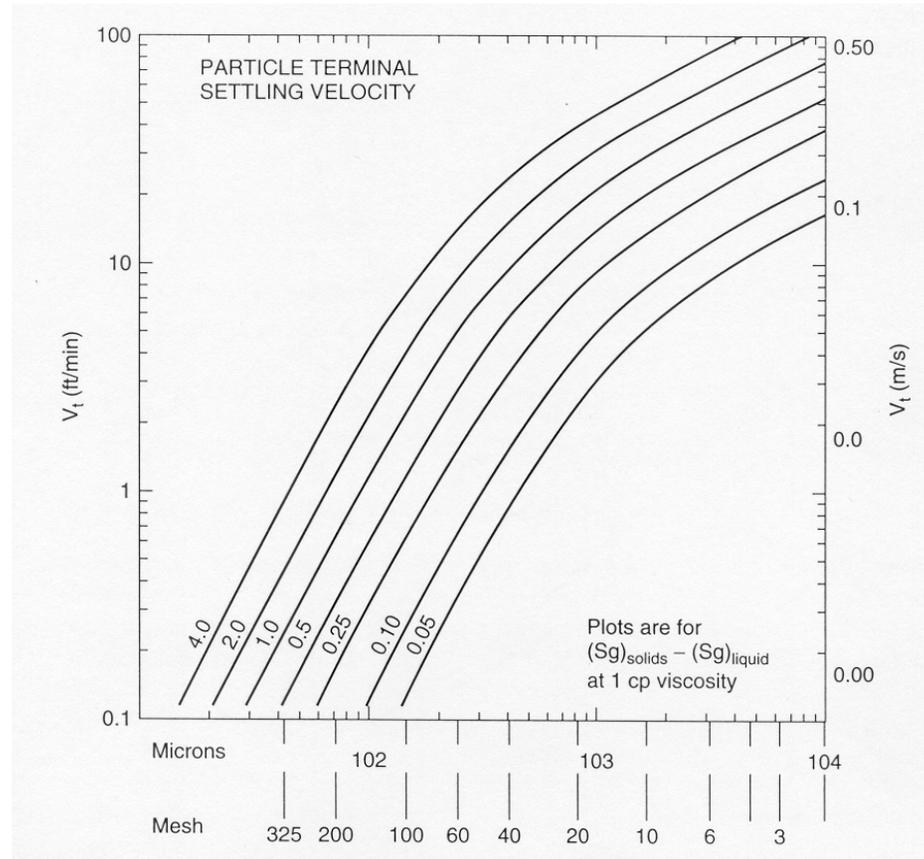


Difficulty

- **Primary factor – settling velocity**
 - with density adjustment
- **Many other factors involved**
 - mixer geometry factors
 - particle property factors
 - fluid property factors



Terminal Settling Velocity





Terminal Settling Velocity

- **Settling due to density difference**
- **Slow settling**
 - laminar
 - Stokes flow
- **Rapid settling**
 - turbulent
 - Newton flow
- **Transition between laminar and turbulent**



Agitated Suspension

- **Not terminal settling velocity**
- **Agitated flow not vertical at all points**
- **Initial suspension by horizontal flow across bottom**
- **Suspension characteristics a stronger function of density than predicted by terminal settling velocity**
- **Density more important than diameter**

Zwietering Correlation

$$N_{js} = S v^{0.1} \left[\frac{g_c (\rho_s - \rho_l)}{\rho_l} \right]^{0.45} X^{0.13} d_p^{0.2} D^{-0.85}$$



Density Effect on Terminal Settling Velocity

$$N_{js} = S' \left[\left(\frac{\rho_s - \rho_l}{\rho_l} \right) u_t \right]^{-0.28}$$

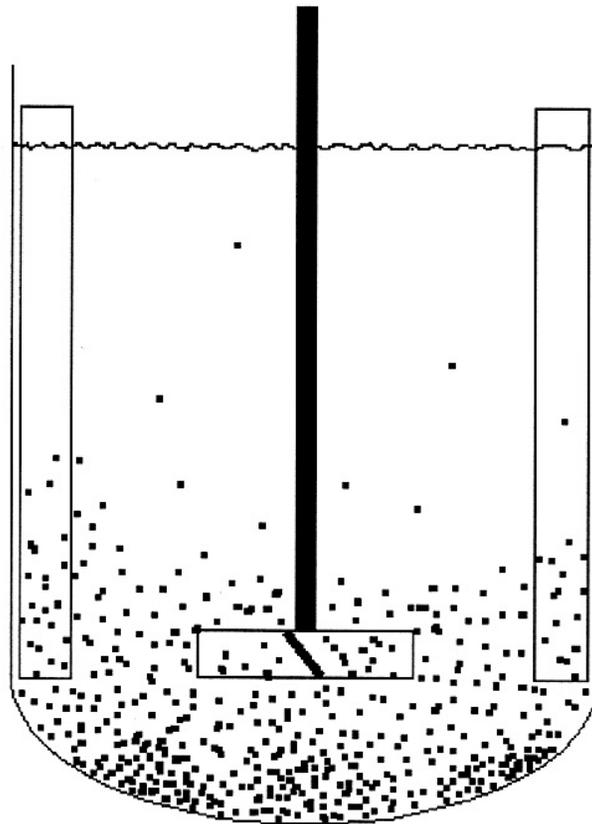


Mixing Intensity

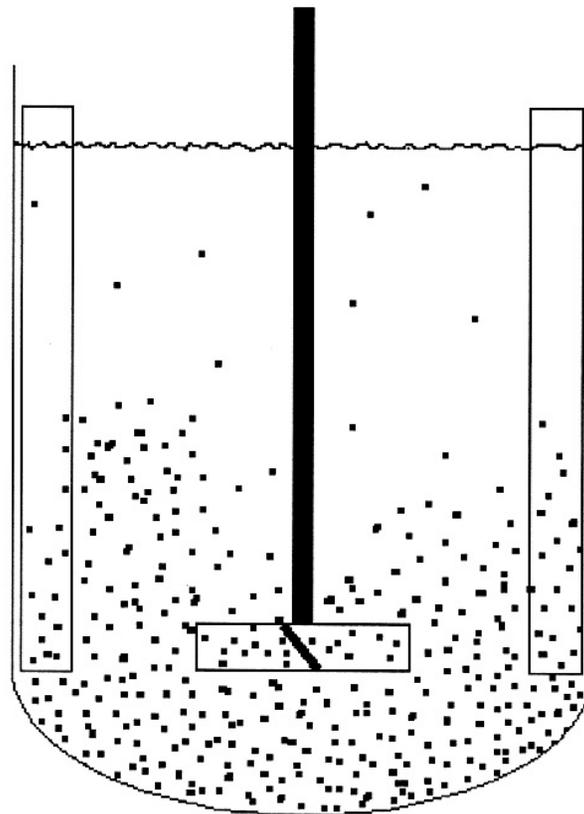
- **On-bottom motion**
 - all particles moving
 - not necessarily suspended
- **Off-bottom suspension**
 - all particles suspended
 - cloud height
- **Uniform suspension**
 - all particles well distributed



On-Bottom Motion

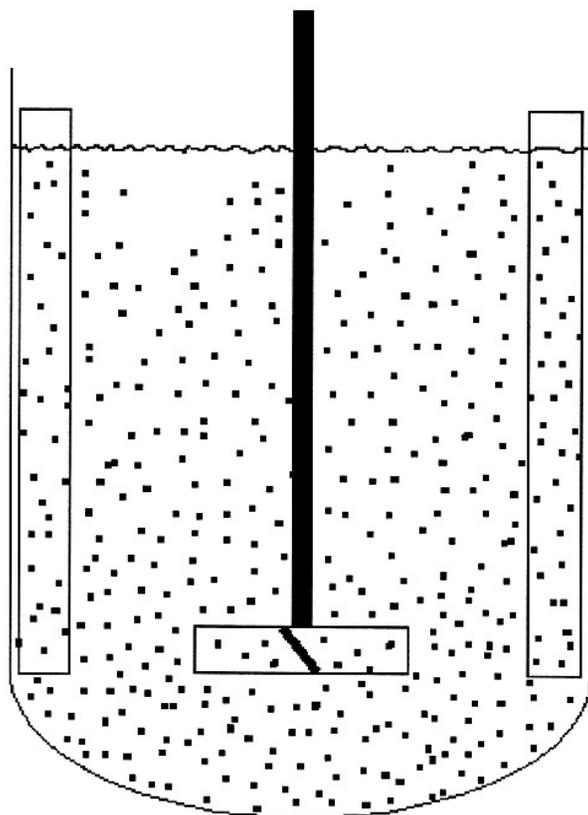


Off-Bottom Suspension



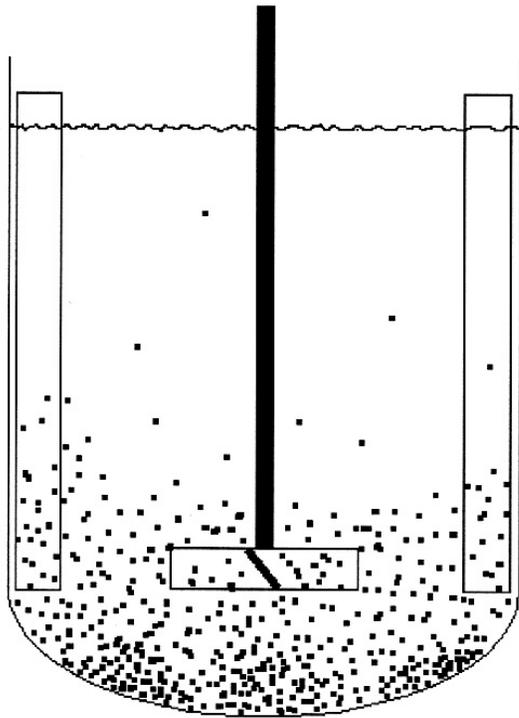


Uniform Suspension

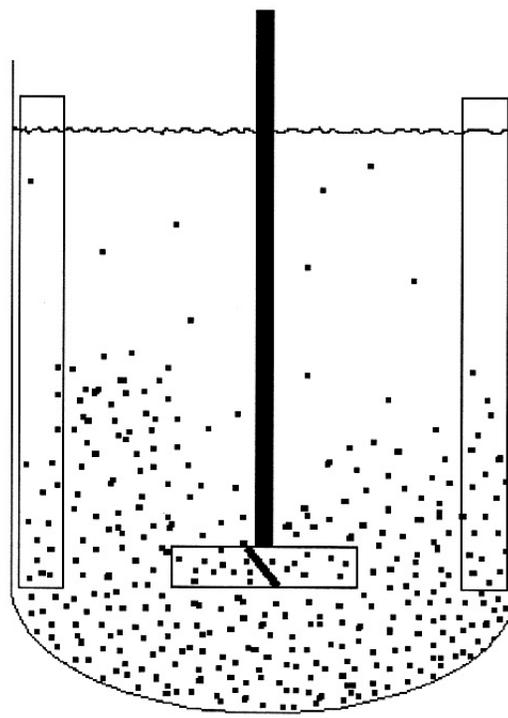




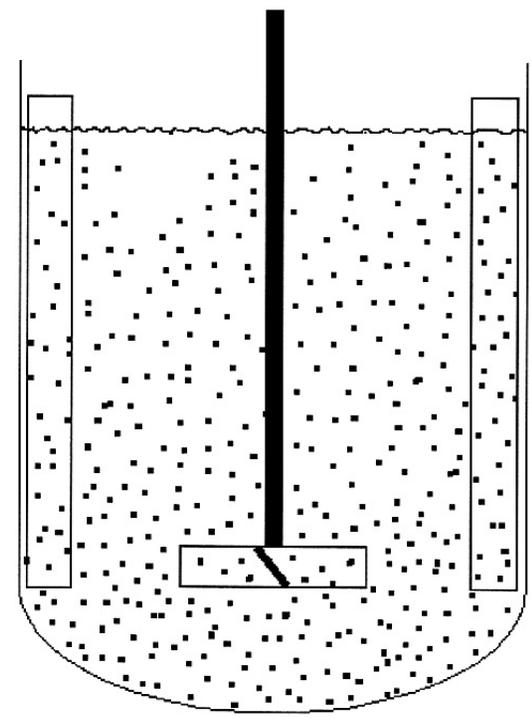
Suspension Levels



On Bottom
Motion



Off-Bottom
Suspension



Complete
Suspension₁₅



Mixer Design Factor

- **Just suspended speed – N_{JS}**
- **Classical correlation by Zwietering**
– adapted for practical use
- **Other more complicated and more accurate correlations**
- **Testing and scale-up – best method**

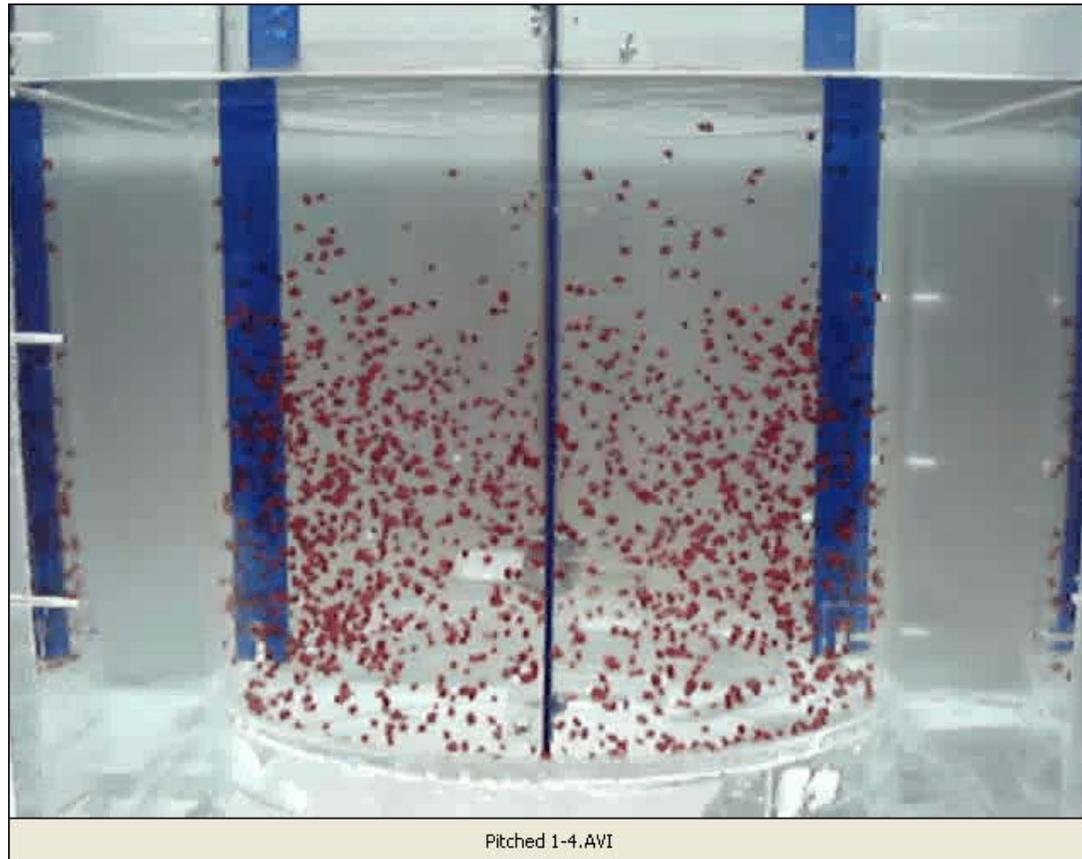


Mixer Geometry Factors

- **Impeller type – axial flow is best**
- **Impeller to tank diameter**
- **Off-bottom clearance**
- **Number of impellers**
- **Liquid level**
- **Baffle length – off-bottom clearance**

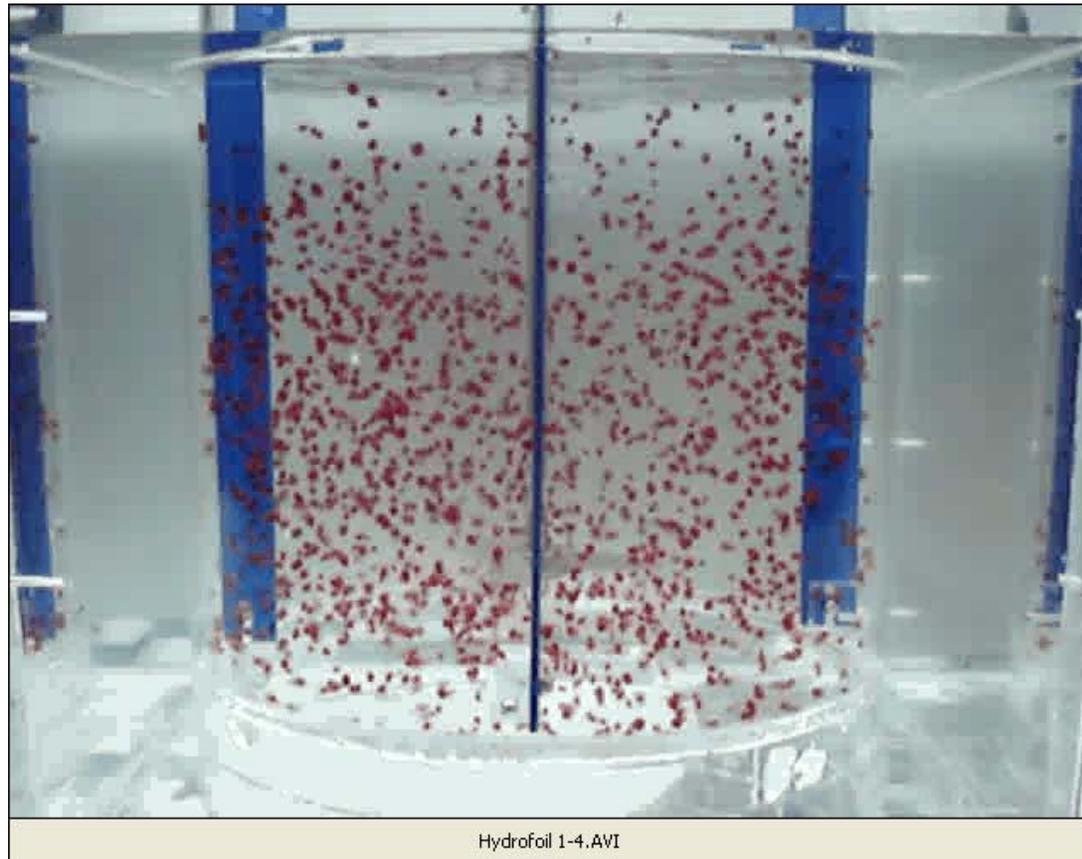


Pitched-Blade Turbine



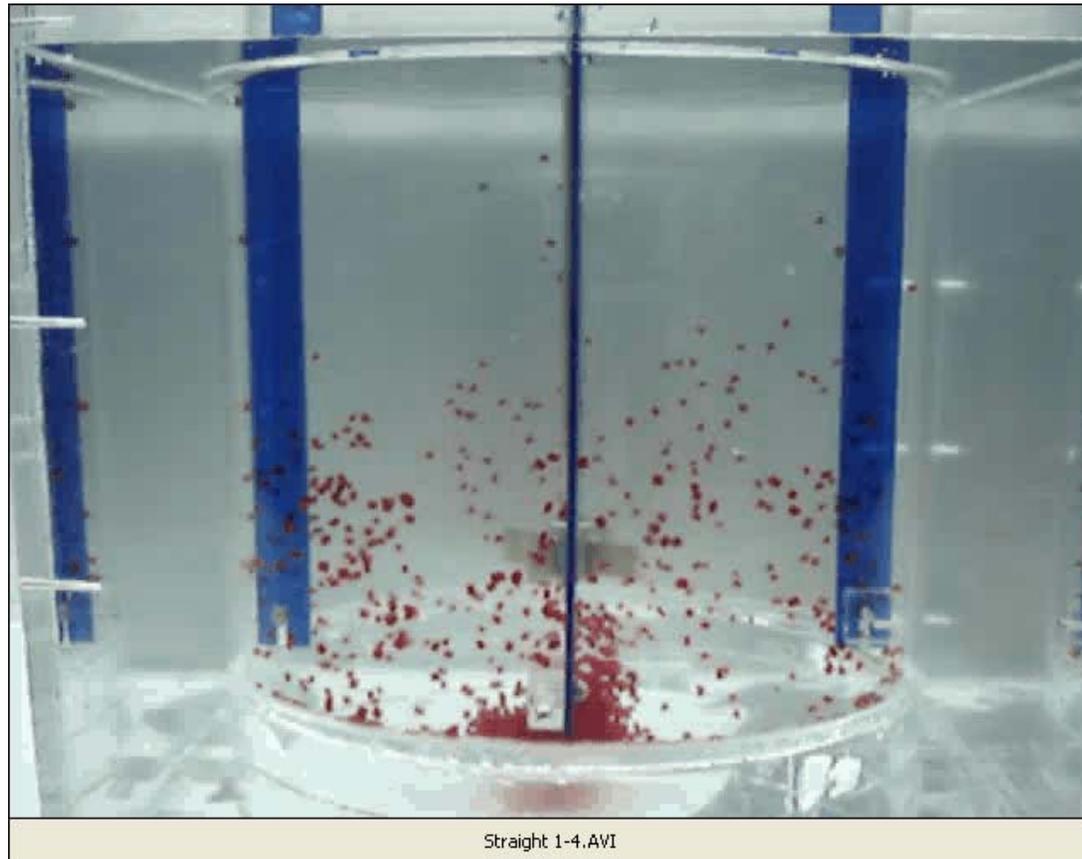


Hydrofoil Impeller





Straight-Blade Turbine



Straight 1-4.AVI

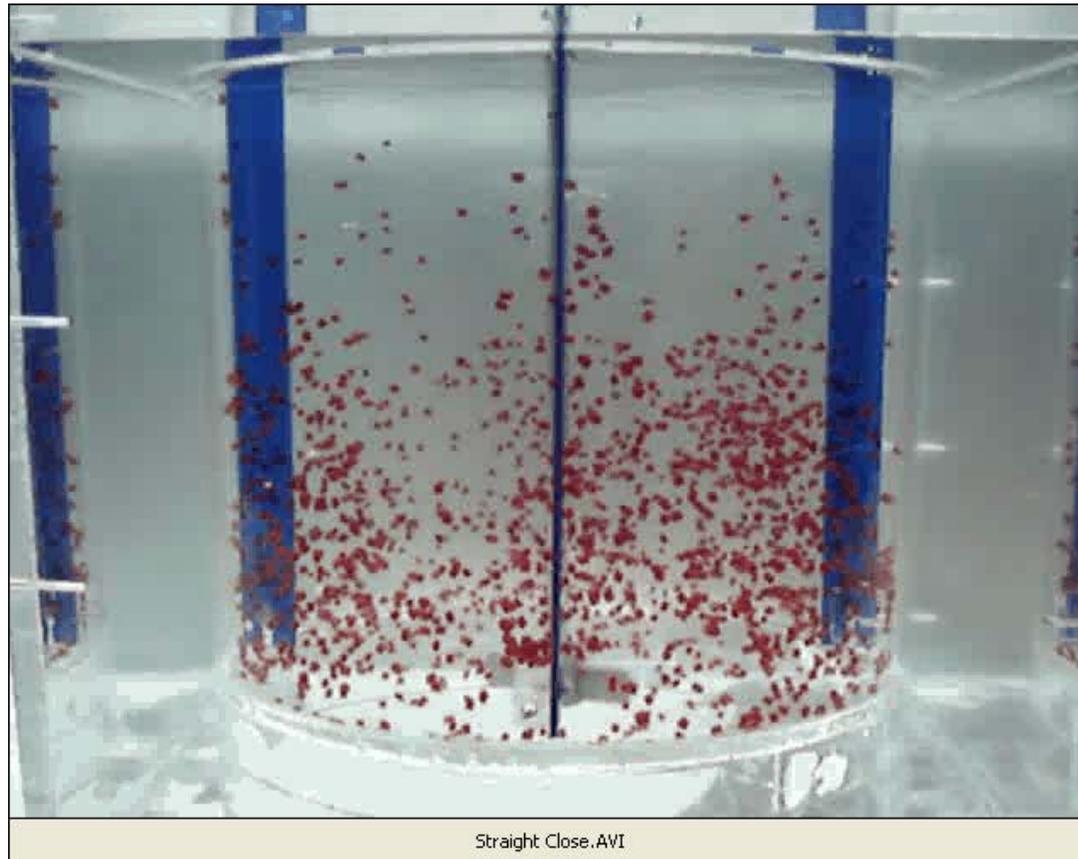


Suspension with Radial Flow

- **The straight-blade radial flow impeller did not work with typical off-bottom clearance**
- **Close clearance does work for solids suspension**
- **Impeller location can be a major factor in solids suspension**



Straight-Blade Turbine – Close Clearance



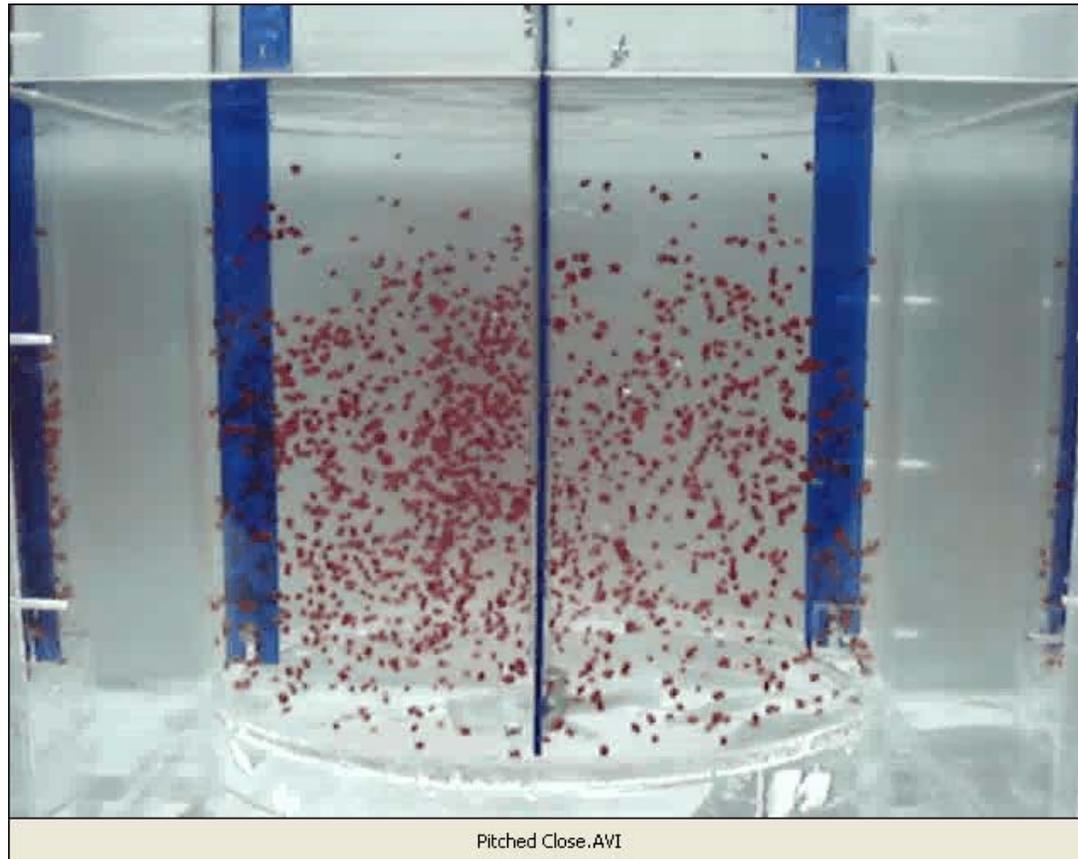


Suspension with Axial Flow

- **Axial flow impellers work at close clearance**
 - pitched-blade turbine
 - hydrofoil impeller
- **Pitched-blade turbine requires less power than straight-blade turbine for the same results**



Pitched-Blade Turbine – Close Clearance



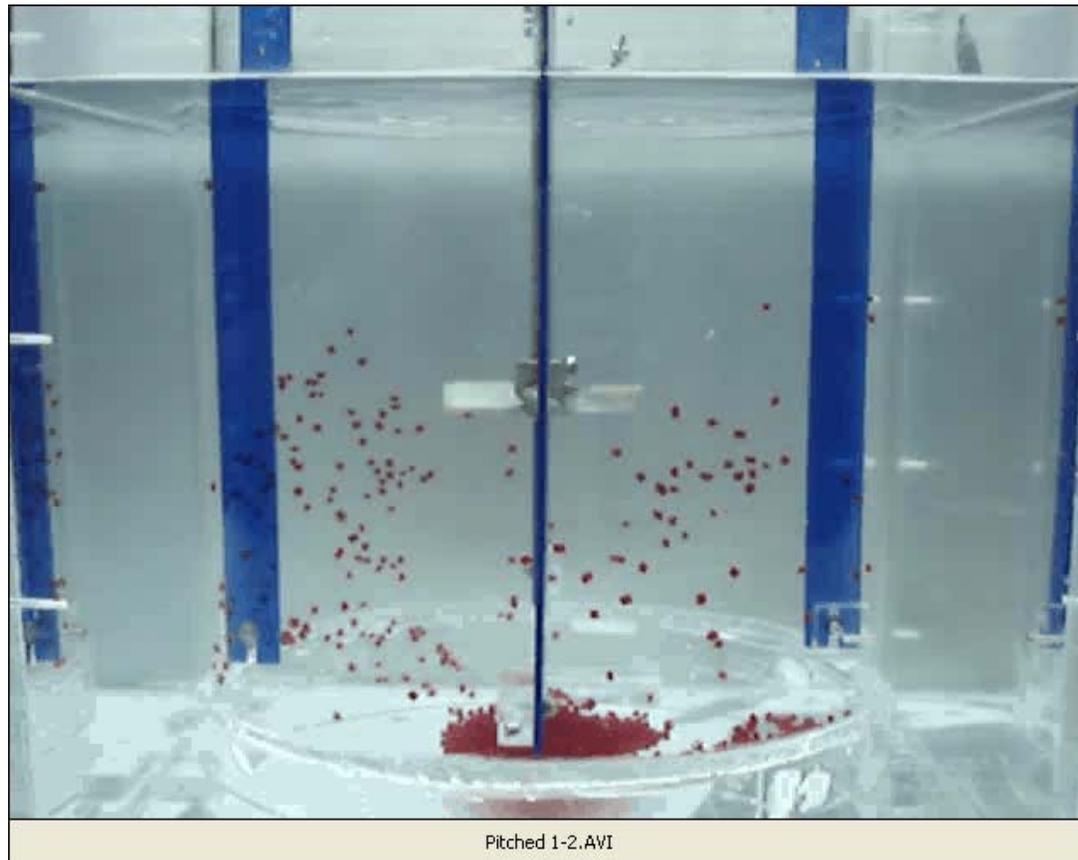


High Clearance Causes Problems

- **Pitched-blade turbine fails to suspend solids when too far off-bottom**
- **Hydrofoil impeller works better even at high clearance position**
- **Different degrees of axial flow are important for solids suspension**

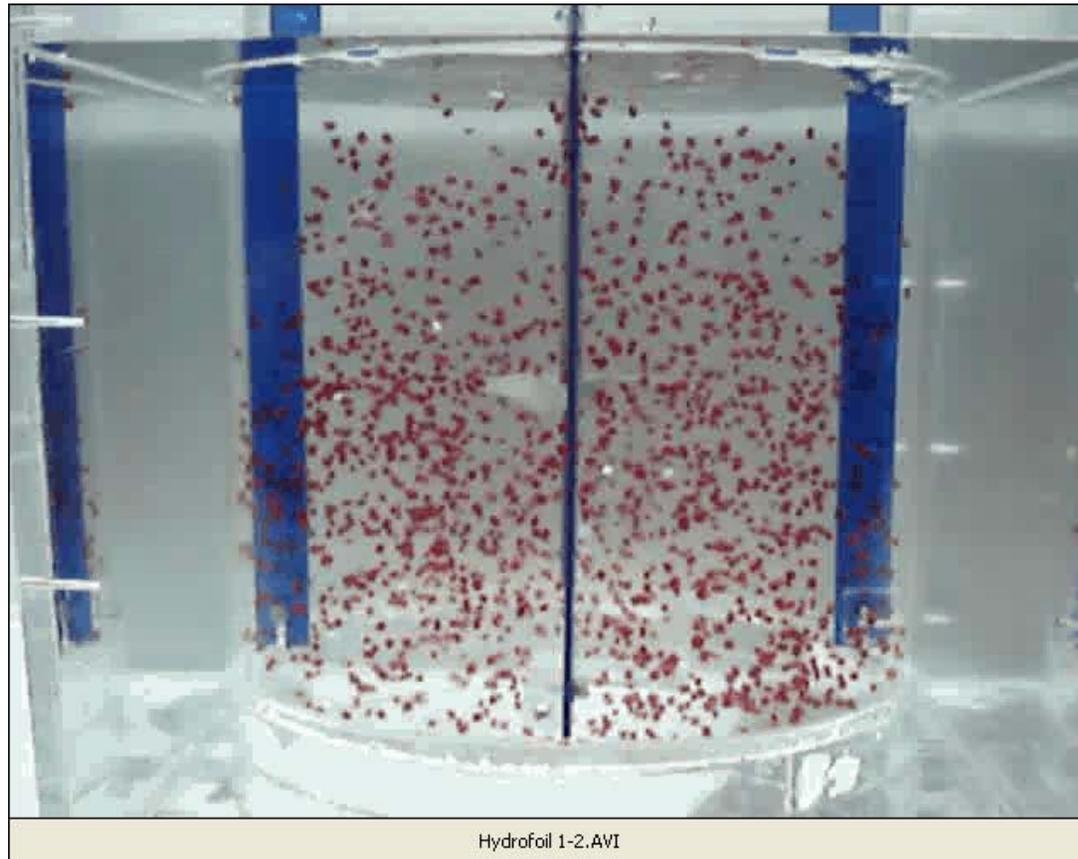


Pitched-Blade Turbine – 1/2 Liquid Level Off-Bottom





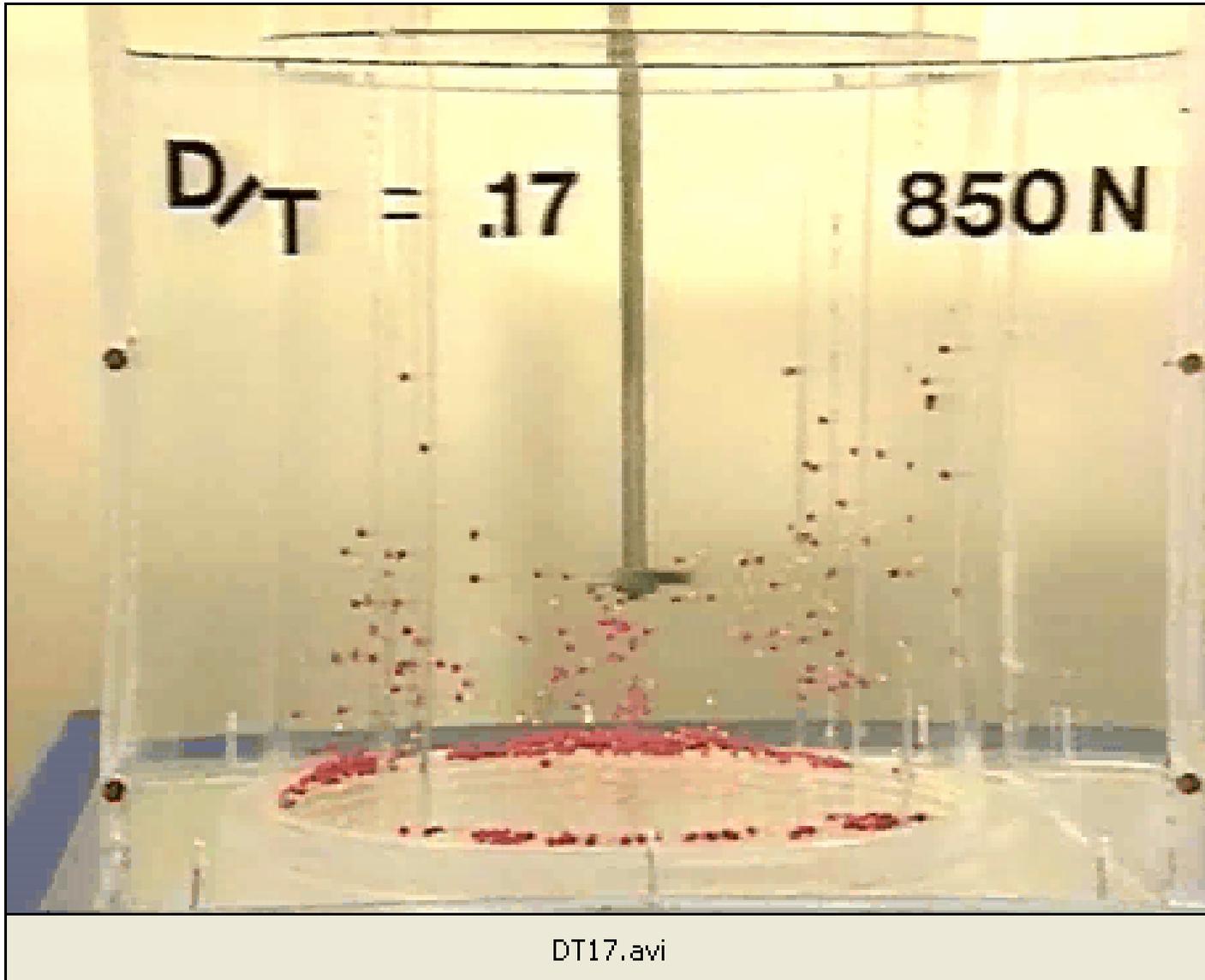
Hydrofoil Impeller – 1/2 Liquid Level Off-Bottom

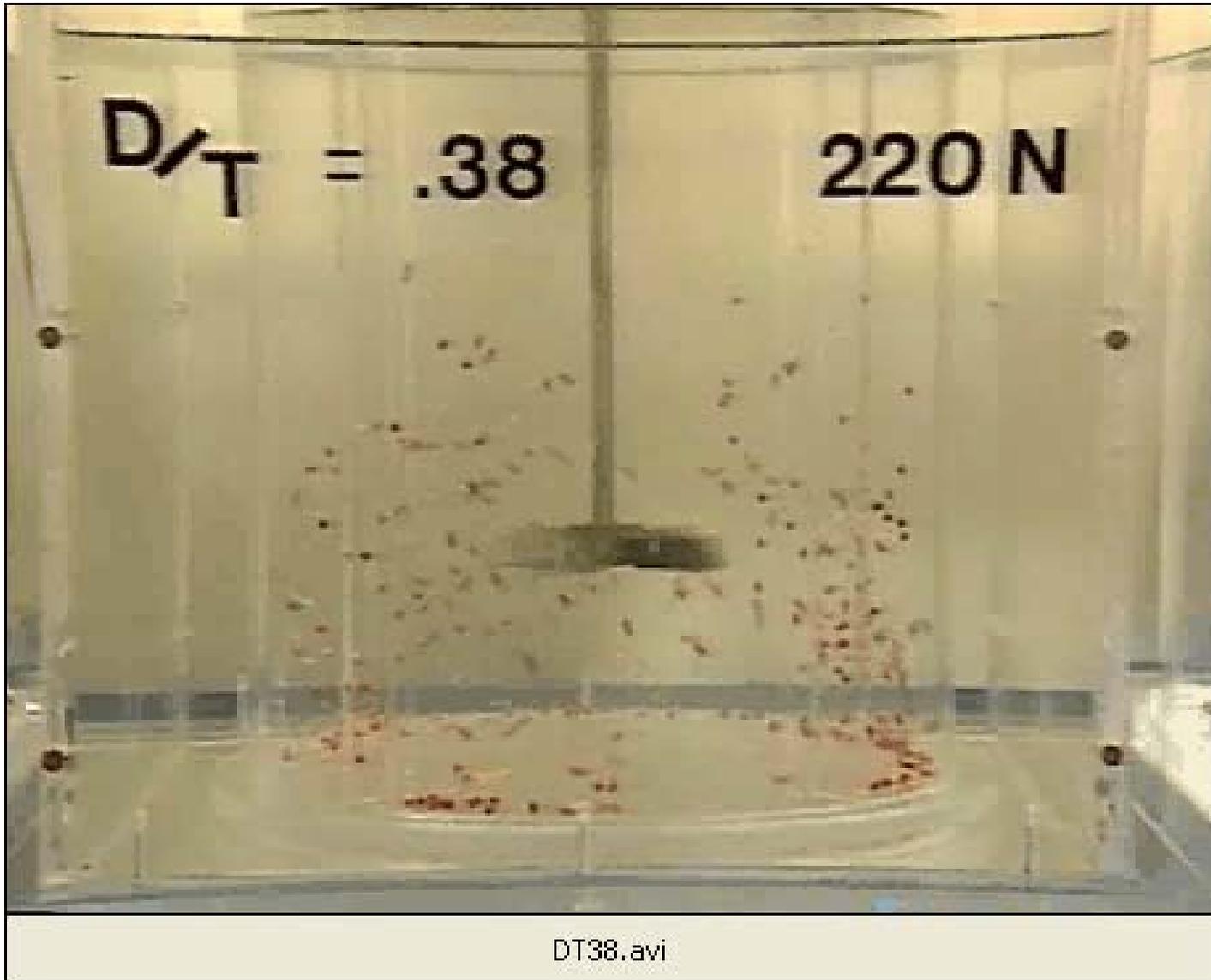


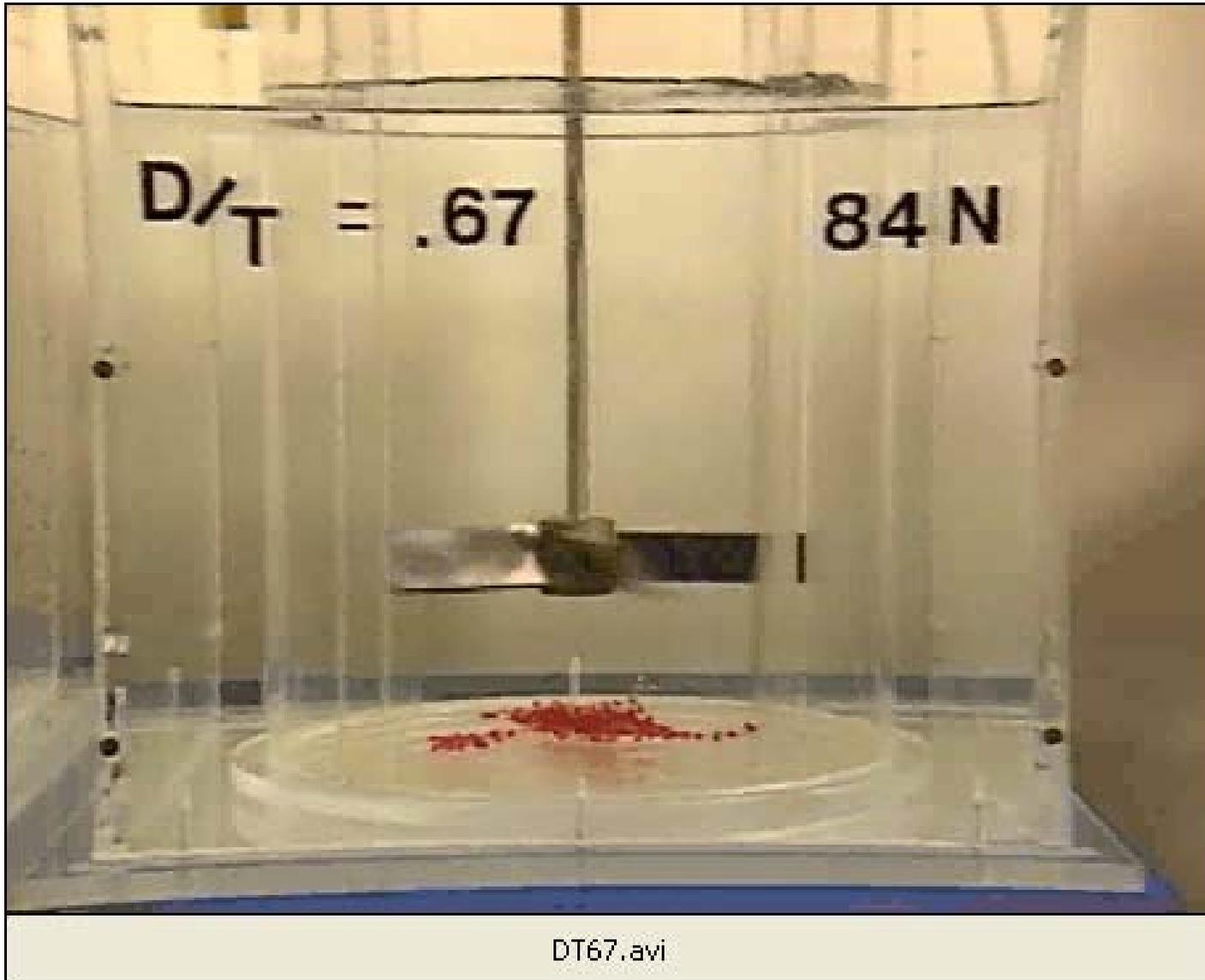


Impeller-to-Tank Diameter Ratio

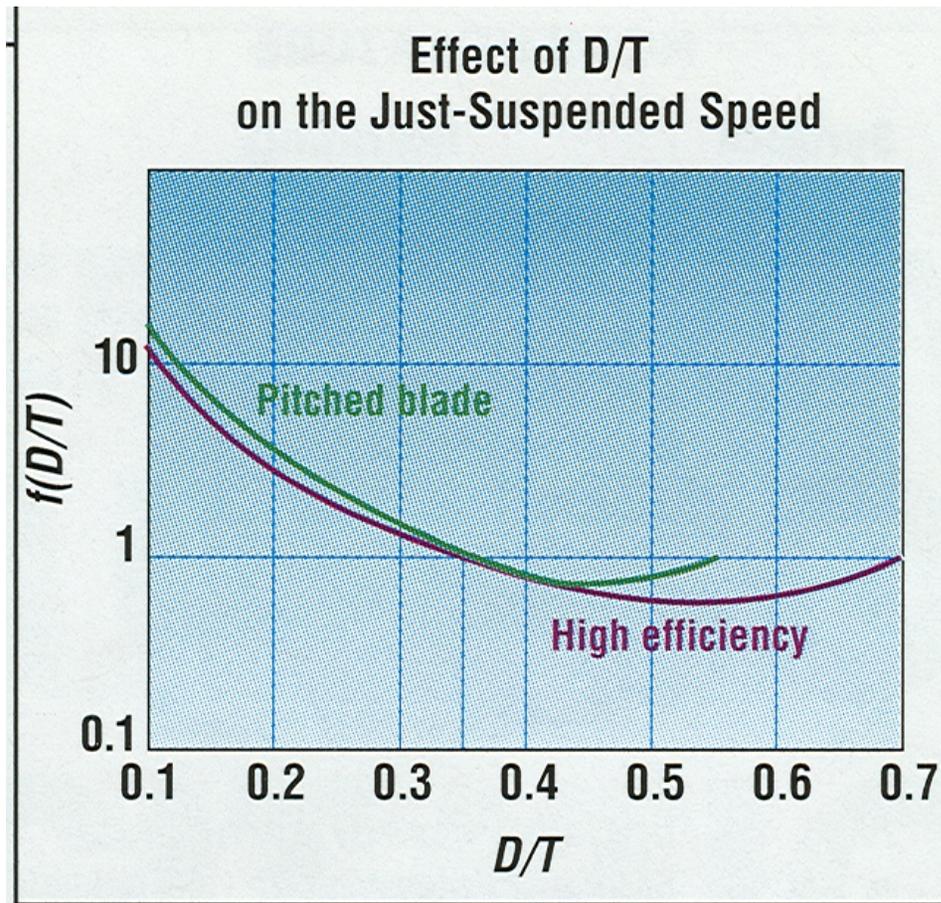
- **Small impellers require more power than larger ones**
- **Definite optimum impeller-to-tank diameter ratio – about 0.4**
- **Large impellers do not sweep the bottom**



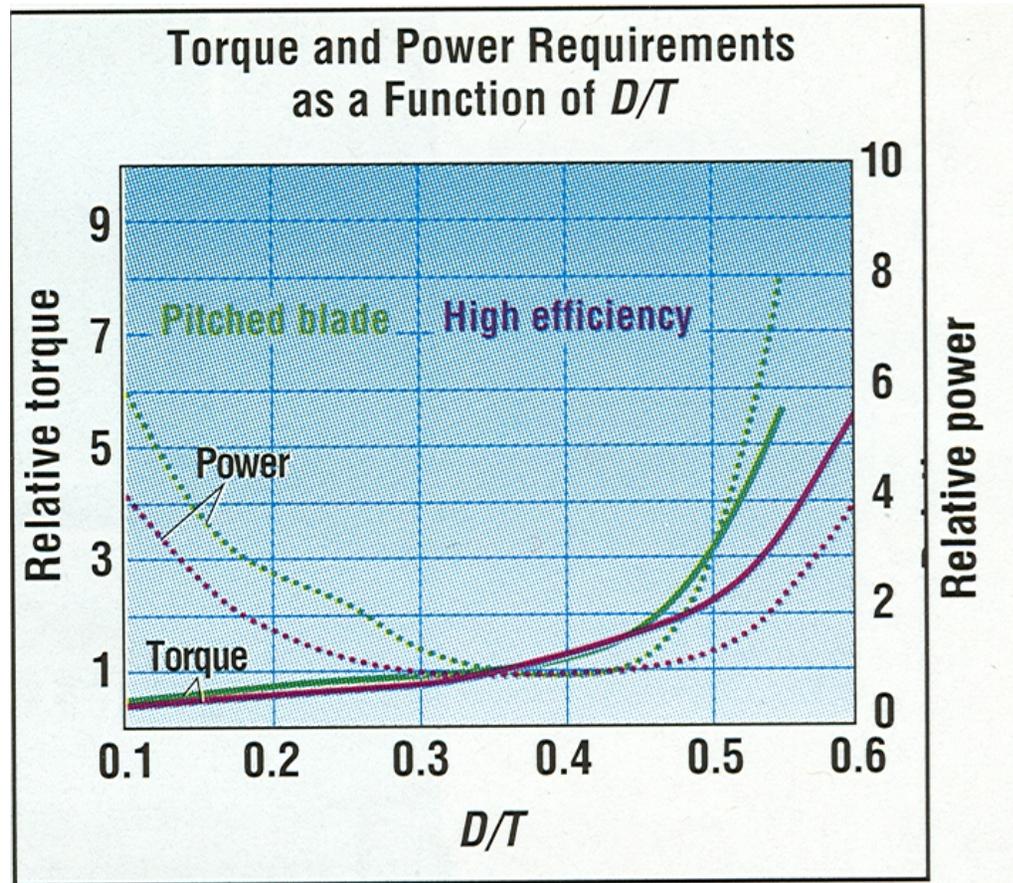




Just Suspended Speed



Power and Torque



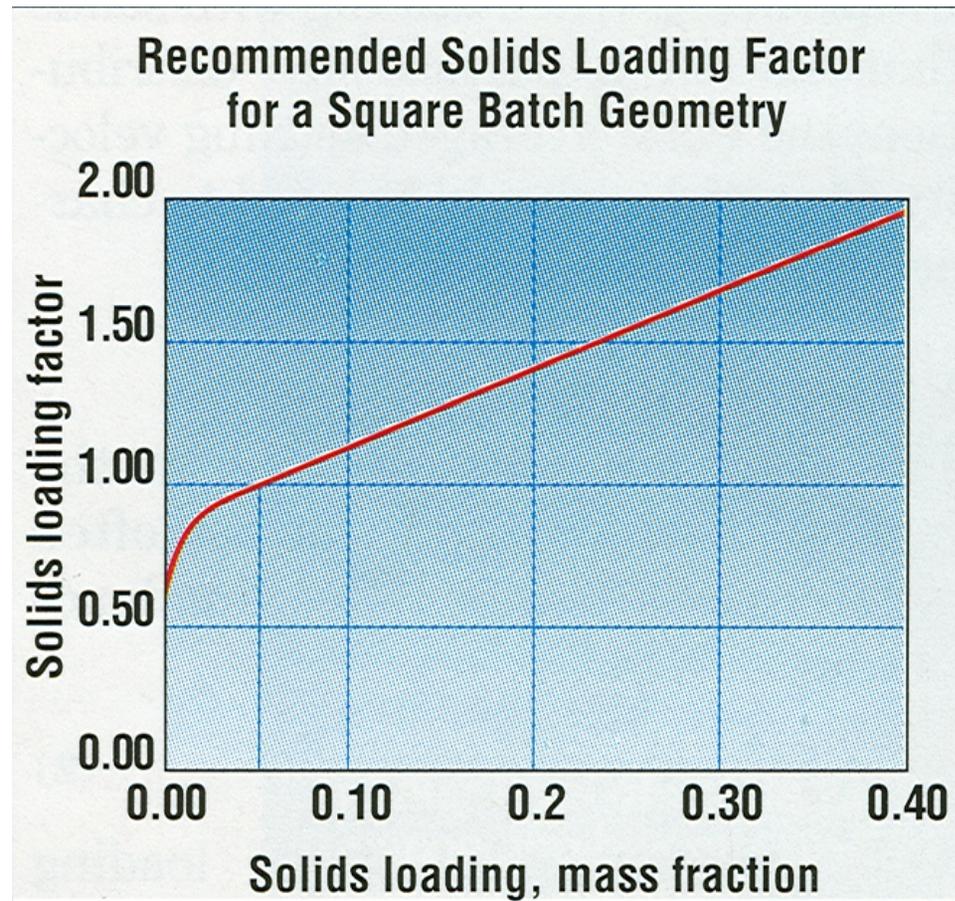


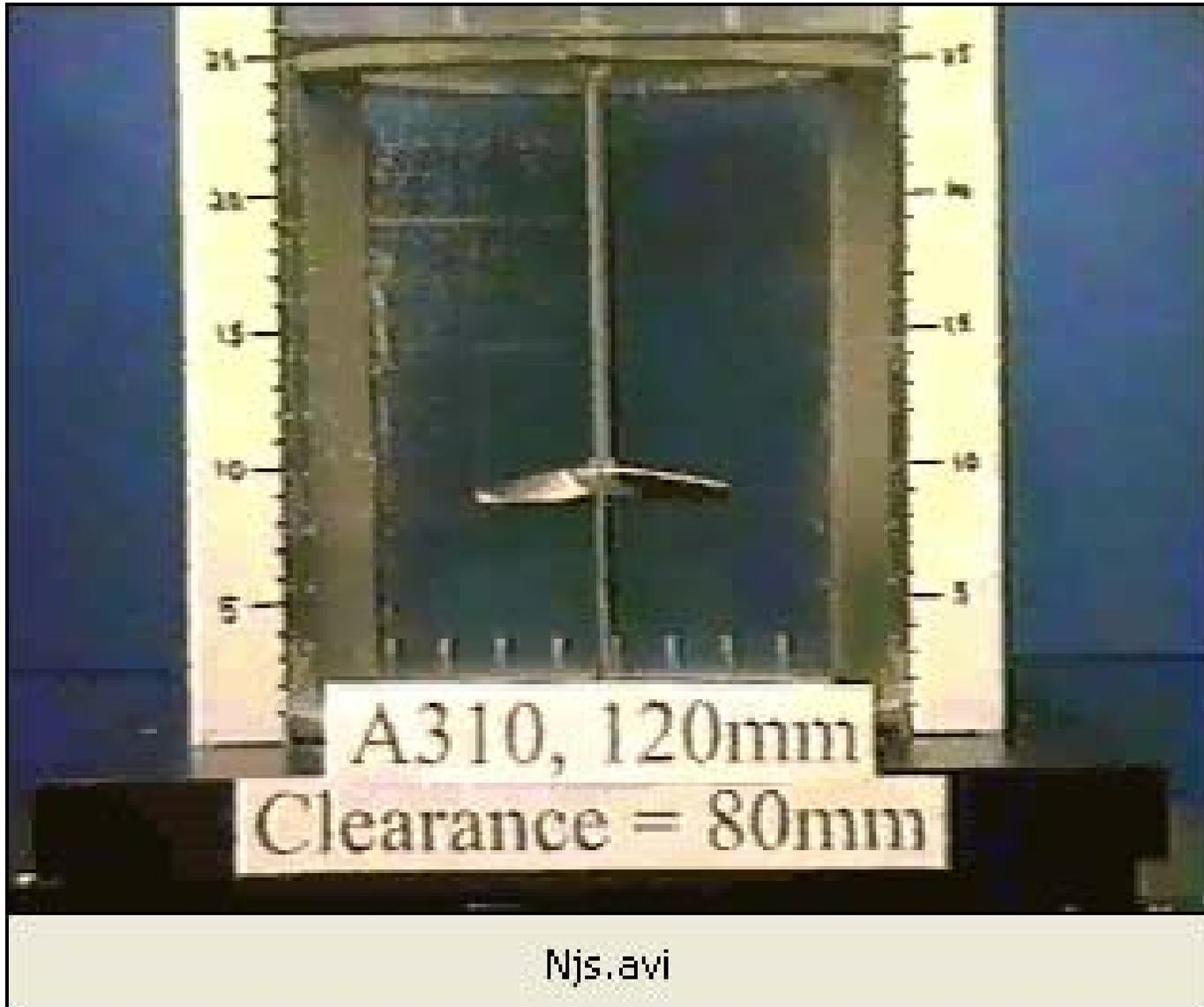
Solids Concentration

- **More solids – more difficult to suspend**
- **Increased concentration – higher speed for same suspension**



Effect of Concentration

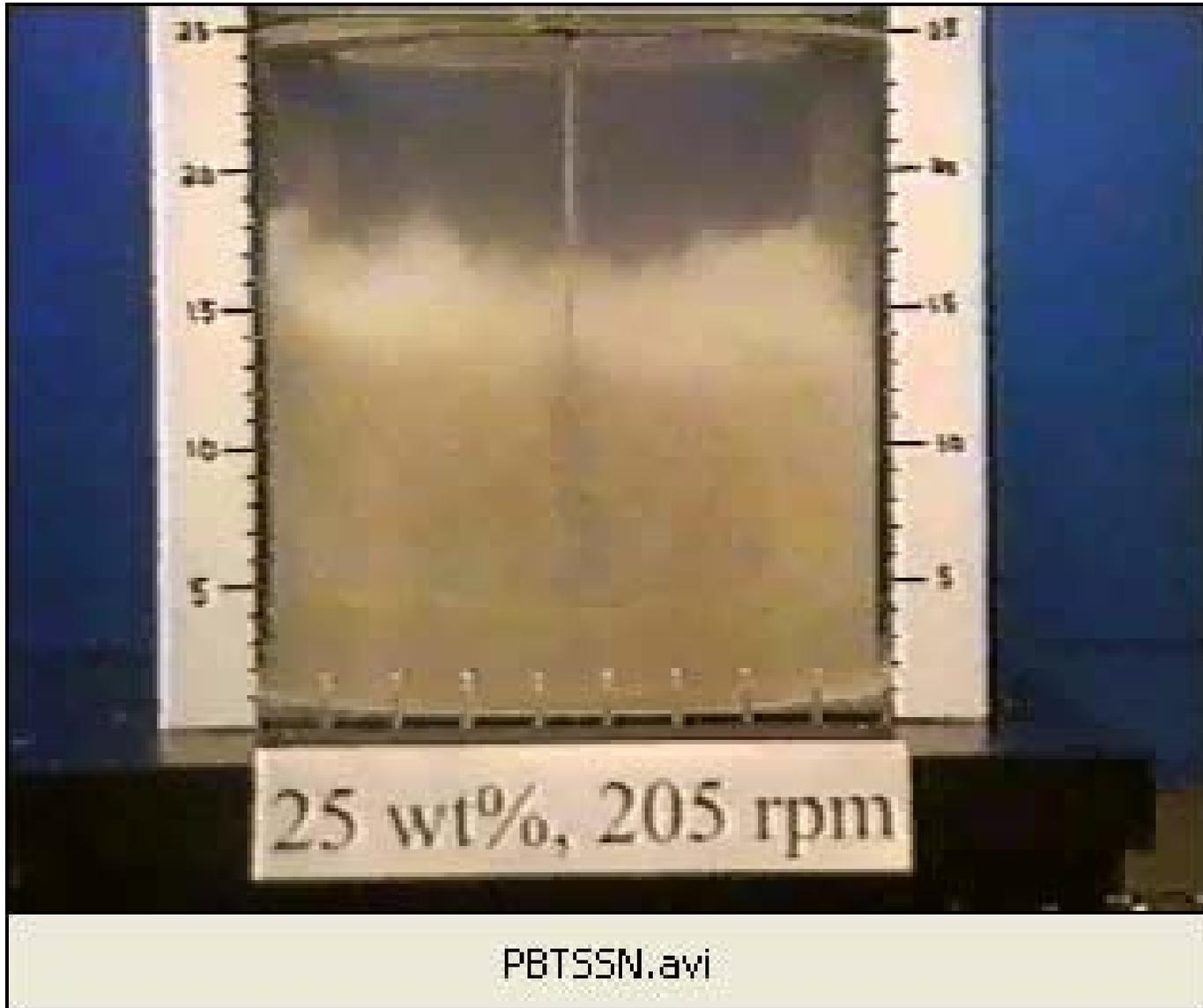






Cloud Height

- **Degree of uniformity**
- **Rapidly settling particles – uniform size distribution**
- **Distinctive cloud appearance**
- **More agitation – higher cloud height**
- **Suspension is never quite uniform**





Similarity and Scale-up

- **Geometric similarity – essential**
- **Kinematic and dynamic similarity – limited benefit**
- **Scale-up by empirical relationships**

Scale-up by Geometric Similarity

- Speed adjustment only
- Large scale speed – less than small scale speed
- Exponent maintains one constant characteristic

$$N_2 = N_1 \left(\frac{D_1}{D_2} \right)^n$$

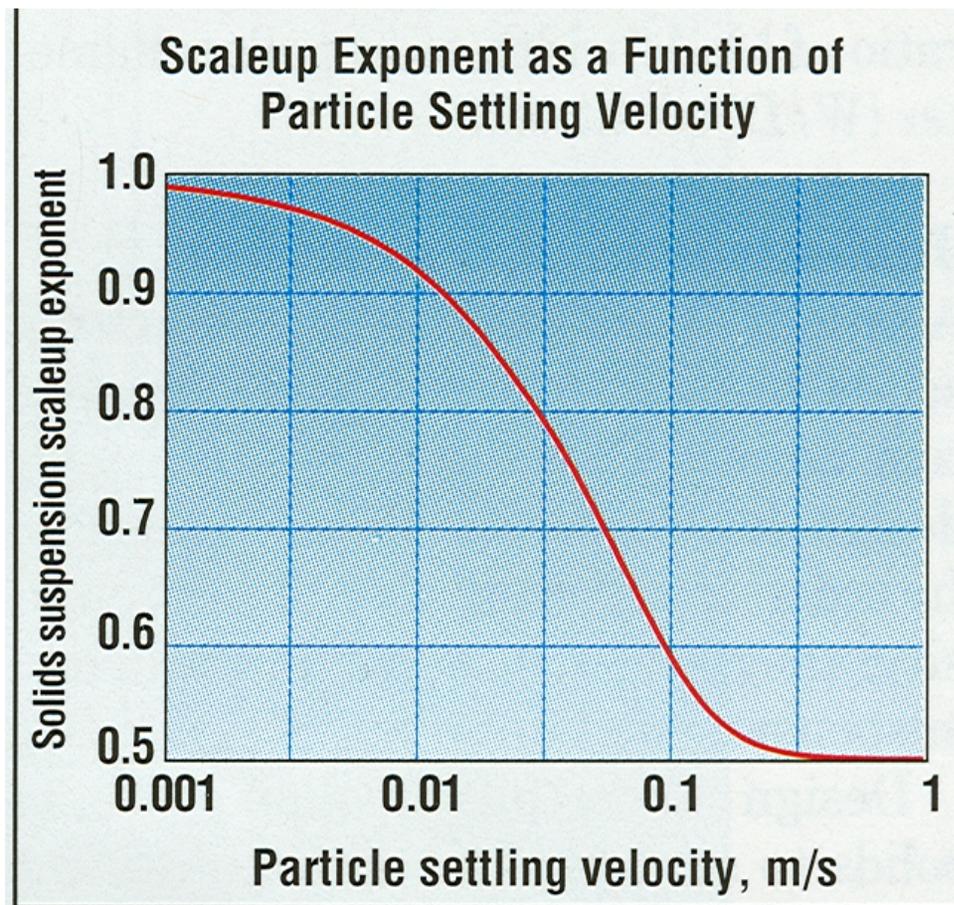


Scale-up Exponent

- **Equal tip speed (fluid velocity)**
 - $n=1$
- **Equal power per volume**
 - $n=2/3$
- **Equal blend time**
 - $n=0$
- **Zwietering suspension**
 - $n=0.85$



Scale-up Solids Suspension





Scale-up

- **Depends on settling velocity**
 - slow settling follows flow
 - rapid settling difficult
- **Scale-up may also depend on size of test**
- **Larger tests less conservative scale-up**



Other Factors

- **Fluid viscosity**
 - 10 to 20 cp more difficult
 - 100 cp easier – no settling
- **Particle shape**
- **Size distribution**



Conclusions

- **Good understanding of solids suspension with mechanical mixers**
- **Understanding of steady jet mixers**
- **Little understanding of the effects of pulse mixing**
 - cycle duration
 - refill period
- **Uncertain scale-up criteria**



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